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(54) **POWER CONVERTER INCLUDING A RECIRCULATING SNUBBER**

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H02M 1/00 (2006.01)

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CPC **H02M 1/34** (2013.01); **H02M 7/06** (2013.01); **H02M 1/0048** (2021.05); **H02M 1/0077** (2021.05); **H02M 1/346** (2021.05)

(58) **Field of Classification Search**

CPC H02M 1/34; H02M 1/342; H02M 1/344; H02M 7/06; H02M 7/062; H02M 1/0048; H02M 1/0051; H02M 1/0077; H02M 1/346

See application file for complete search history.

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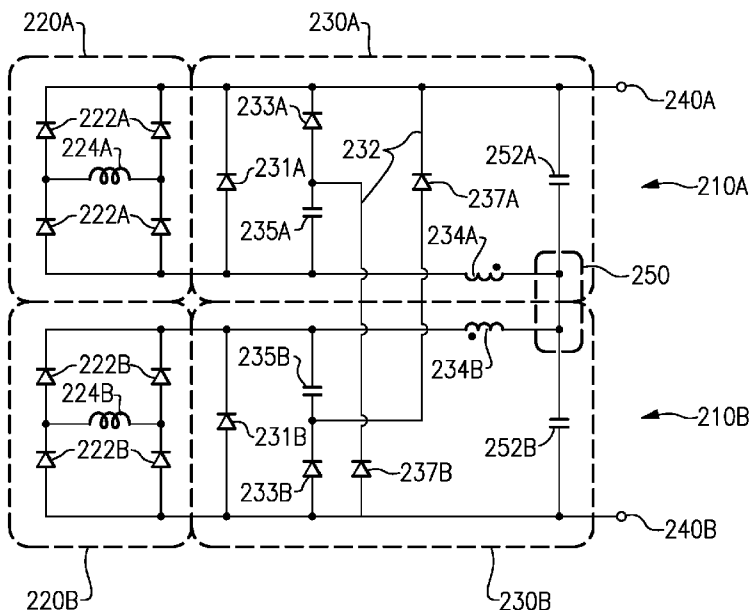
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(57) **ABSTRACT**

A power converter includes a first rectifier circuit having a pair of first rectifier circuit output terminals and a second rectifier circuit having a pair of second rectifier circuit output terminals, a snubber circuit comprising a first diode and a first capacitor connected to each other at a first node and connecting the pair of first rectifier circuit output terminals, a second diode and a second capacitor connected to each other at a second node and connecting the pair of second rectifier circuit output terminals, a third diode connecting the first node to one of the pair of second rectifier circuit output terminals, and a fourth diode connecting the second node to one of the pair of first rectifier output terminals.

15 Claims, 2 Drawing Sheets



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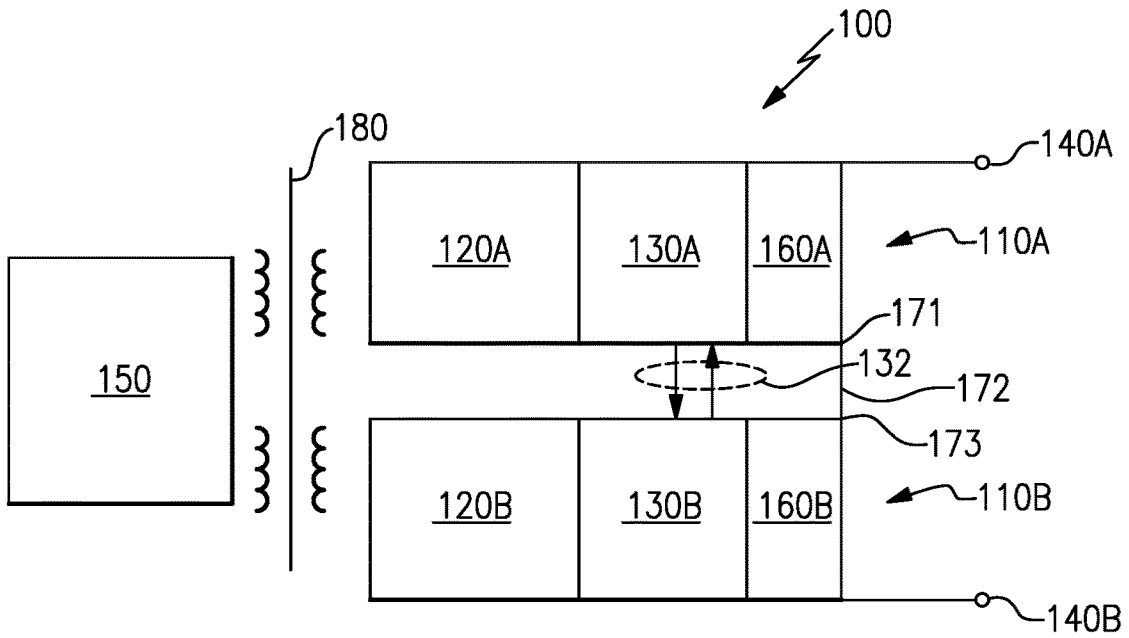


FIG. 1

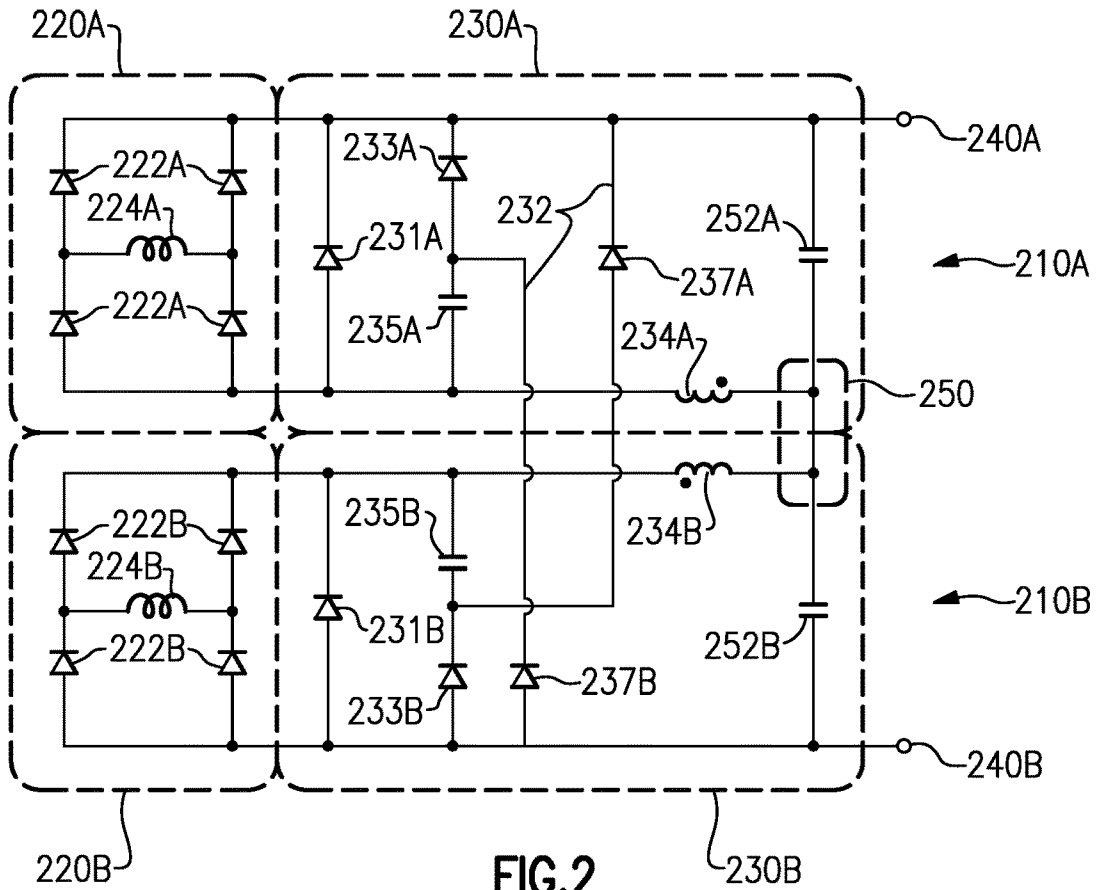


FIG. 2

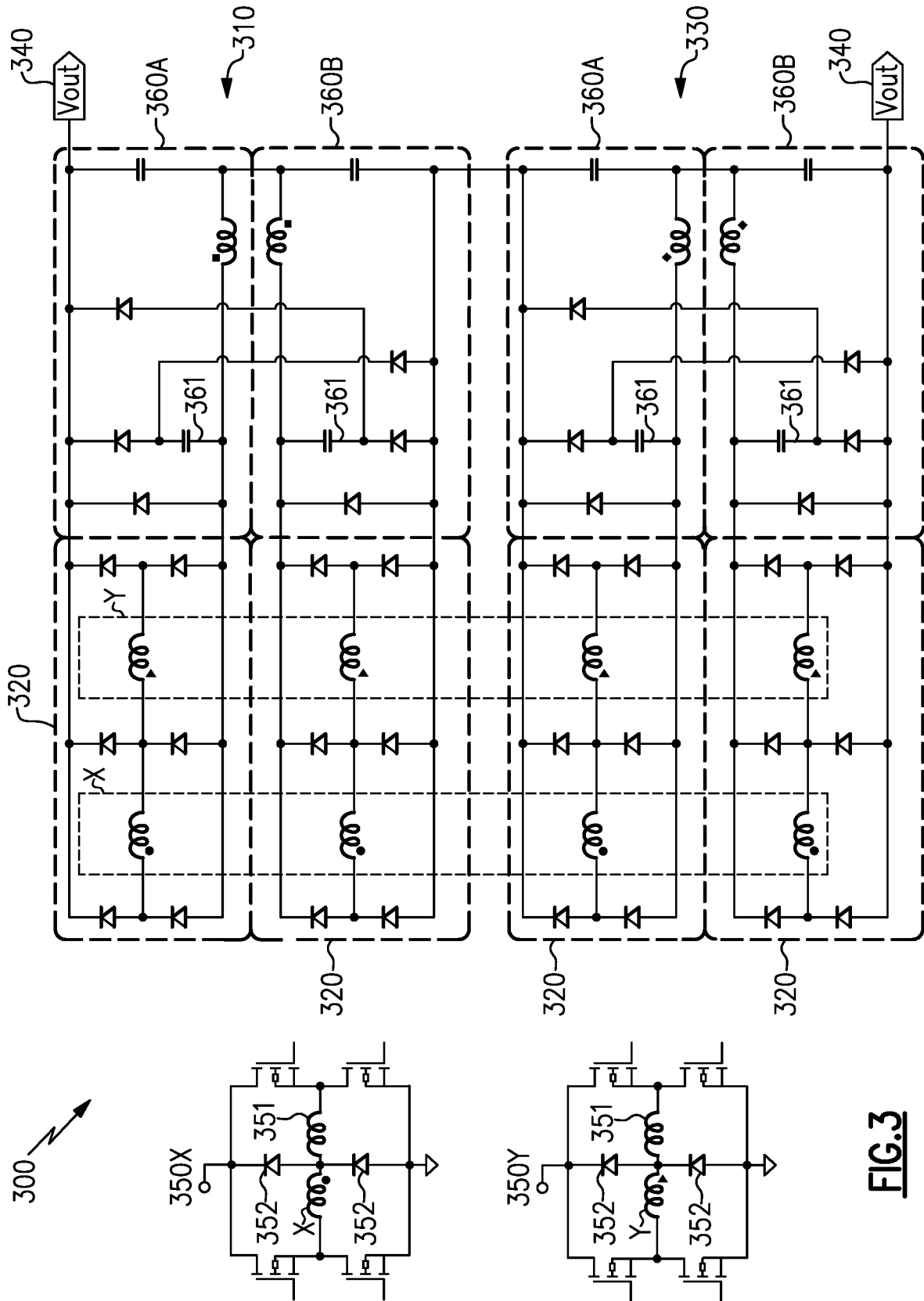


FIG. 3

POWER CONVERTER INCLUDING A RECIRCULATING SNUBBER

STATEMENT REGARDING FEDERALLY SPONSORED RESEARCH OR DEVELOPMENT

This invention was made with government support under contract number NNC16CA21C awarded by NASA. The government has certain rights in the invention.

TECHNICAL FIELD

The present disclosure relates generally to power converters, and more particularly to power converters including a recirculating snubber circuit.

BACKGROUND

Electrical power converters are used in multiple applications to convert power from a first set of voltage and current characteristics to a second set of voltage and current characteristics. Use of the power converters allows a single power source, such as a battery or other stored energy component, to power multiple different electronic components each of which may have a different power requirement.

One exemplary type of power converter, referred to as a step-up converter, includes multiple stacked rectifier sections in order to achieve a higher output voltage. Each of the rectifier sections includes a bridge rectifier, as well as circuitry connecting the bridge rectifier to a voltage output. Previous high-voltage bridge rectifiers have been constructed utilizing silicon carbide diodes. However silicon carbide based diodes are not suitable for usage in some environments, such as outer space, due to their sensitivity to radiation.

SUMMARY OF THE INVENTION

In one exemplary embodiment a power converter includes a first rectifier circuit having a pair of first rectifier circuit output terminals and a second rectifier circuit having a pair of second rectifier circuit output terminals, a snubber circuit comprising a first diode and a first capacitor connected to each other at a first node and connecting the pair of first rectifier circuit output terminals, a second diode and a second capacitor connected to each other at a second node and connecting the pair of second rectifier circuit output terminals, a third diode connecting the first node to one of the pair of second rectifier output terminals, and a fourth diode connecting the second node to one of the pair of first rectifier output terminals.

In another example of the above described power converter the first capacitor is connected to the one of the pair of first terminals not connected to the third diode and the second capacitor is connected to the one of the pair of second terminals not connected to the fourth diode.

In another example of any of the above described power converters a filter circuit includes a first filter inductor connecting the one of the pair of first terminals not connected to the third diode to a midpoint node, and a second filter inductor connecting the one of the pair of second terminals not connected to the fourth diode to the midpoint node.

In another example of any of the above described power converters each of the first rectifier circuit and the second rectifier circuit are one of a full bridge rectifier and a center tapped rectifier.

In another example of any of the above described power converters the each of the first rectifier and the second rectifier comprises a plurality of silicon diodes.

In another example of any of the above described power converters each of the first rectifier circuit and the second rectifier circuit rectify currents from transformers driven by a multi-phase power system.

In another example of any of the above described power converters each of the first rectifier circuit and the second rectifier circuit is substantially identical to each other pair of rectifier sections.

An exemplary method for reducing voltage spikes in a power converter includes recirculating snubber energy through a snubber circuit comprising a first diode and a first capacitor connected to each other at a first node and connecting the pair of first rectifier circuit output terminals, a second diode and a second capacitor connected to each other at a second node and connecting the pair of second rectifier circuit output terminals, a third diode connecting the first node to one of the pair of second rectifier output terminals, and a fourth diode connecting the second node to one of the pair of first rectifier output terminals.

Another example of the above described method for reducing voltage spikes in a power converter further includes filtering a voltage between a high voltage output node and a low voltage output node using a third capacitor connecting the high voltage output node to a midpoint node and a fourth capacitor connecting the low voltage output node to the midpoint node.

In another example of any of the above described exemplary methods for reducing voltage spikes in a power converter the first capacitor and the second capacitor have approximately the same capacitance.

Another example of the above described power converters having a multiphase power system includes drivers that may be selectively operated in a pulse width modulated mode or a phase shifted bridge mode.

In another example of the above described power converters, each rectifier receives power from at least one transformer that has a primary winding.

In another example of the above described power converters, the voltage across each primary winding is limited by clamping diodes.

These and other features of the present invention can be best understood from the following specification and drawings, the following of which is a brief description.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 illustrates a power converter including multiple stacked rectifier sections.

FIG. 2 schematically illustrates exemplary mirrored rectifier sections such as could be utilized in conjunction with FIG. 1.

FIG. 3 schematically illustrates an alternate mirrored rectifier section for utilization in a dual full bridge converter.

DETAILED DESCRIPTION OF AN EMBODIMENT

FIG. 1 schematically illustrates a power converter 100 including multiple stacked rectifier sections 110A and 110B. Each of the rectifier sections 110A and 110B includes a bridge circuit 120A and 120B constructed of diodes (see 220A and 220B in FIG. 2) connected to a snubber circuit 130A and 130B, a voltage output 140A and 140B, and an output filter 160A and 160B. Paired with the rectifier sec-

tions is a corresponding driver **150** that drives current through transformer **180** to the bridge rectifier sections **110A** and **110B**. Driver **150** can be a single driver or multiple drivers, depending on the needs of a given application. Similarly, the transformer **180** can be a single transformer or multiple transformers, depending on the needs of the given application.

The rectifier sections **110A** and **110B** are mirrored, and include a snubber recirculation circuit **132** configured to pass a snubber current from each snubber section **130A** or **130B** to a corresponding mirrored snubber circuit **130B** or **130A**. In order to make the bridge rectifier rad-hard (more resistant to radiation), a bridge rectifier can be constructed utilizing silicon based diodes instead of other diodes such as those made of silicon carbide. Silicon based diodes, however, have a longer switch-off time, referred to as a reverse recovery time, and can cause spikes in the output voltage of the bridge rectifiers. The snubber circuits **130A** and **130B** operate to limit the amplitude of the spikes in the output voltage of the rectifier circuits **120A** and **120B**.

Snubber circuits **130A** and **130B** mitigate the voltage spikes caused by the reverse recovery time of the diodes in the rectifier circuits **120A** and **120B**. Some existing snubber circuits mitigate the voltage spikes by dissipating substantial amounts of power, resulting in the generation of substantial amounts of heat energy. In space applications, as well as any similar environment, the dissipation of the heat energy is difficult.

Some alternative snubber circuits mitigate the reverse recovery time by recycling the energy. These types of snubber circuits are referred to as "lossless" snubber circuits, despite some small amount of energy dissipation. Some lossless snubber circuits utilize an active switching of one or more transistors within the snubber circuit, and require active controls, which add complexity to the overall system.

In yet further existing lossless snubber circuits, additional inductors are incorporated to allow for passive snubbing, however this increases the weight and cost of the snubber circuit.

In contrast to the existing examples, the mirrored snubber circuits **130A** and **130B** of FIG. 1 avoid the need for added transistors or inductors by utilizing a mirrored construction. The output filter circuits **160A** and **160B** are mirrored with respect to output filter inductor connections (see FIG. 2) such that the output filter inductor of filter circuit **160A** is connected to a low voltage connection of rectifier circuit **120A** and the output inductor of filter circuit **160B** is connected to the high voltage connection of rectifier circuit **120B**. An output inductor of one filter section **160A** is connected to the negative output terminal **171** of the rectifier section **130A** being connected to a midpoint node **172**. The output inductor of the other of the rectifier sections **110B** is connected to the positive output terminal **173** of the rectifier section **130B** being connected to the midpoint node **172**. This configuration can alternately be referred to as being connected in series between output terminals **140**, with the high voltage output of one being connected to the low voltage output of the other, in order to increase the output voltage across the output terminals **140**.

With continued reference to FIG. 1, FIG. 2 schematically illustrates rectifier sections **210A**, **210B**, such as could be used for the rectifier sections **110A**, **110B** of FIG. 1, in more detail. As with FIG. 1, each of the rectifier sections **210A**, **210B** includes a diode bridge portion constructed of multiple diodes **222A**, **222B** arranged in a full bridge configuration about a transformer coil **224A**, **224B**. In alternative configurations, the full bridge rectifiers **220A**, **220B** can be

replaced with alternative rectifier types, such as center-tapped rectifiers and the like. Similarly, the corresponding full bridge driver **150** (see FIG. 1) could be replaced with any other type of driver.

Each of the rectifier sections **210A**, **210B** further includes a snubber/filter circuit **230A**, **230B**. In some cases, such as the illustrated example, a diode **231A**, **231B** can be included parallel to the snubber/filter circuit **230A**, **230B**. The diode **231A**, **231B** is a freewheeling diode that improves the power converter efficiency by reducing power losses during the time intervals when the transformer output voltage is zero. Parallel to the first diode **231A**, **231B** is a snubber diode **233A**, **233B** and snubber capacitor **235A**, **235B** connected in series with each other and connecting the positive and negative outputs of the bridge circuit **220A**, **220B**. As the rectifier sections **210** are mirrored relative to each other, the order of the snubber diode **233A**, **233B** and the snubber capacitor **235A**, **235B** in the two snubber/filter circuits **230A**, **230B** is reversed, with the snubber diode **233A**, being connected to a high side in the first (upper) snubber/filter circuit **230A**, and the snubber diode **233B** being connected to the low side in the second (lower) snubber/filter circuit **230B**.

A node connecting each snubber diode **233A**, **233B** to the corresponding snubber capacitor **235A**, **235B** is connected to the opposite snubber/filter circuit **230A**, **230B** of the opposite rectifier section **210A**, **210B** via the recirculation circuit **232** comprised of snubber diodes **237A** and **237B**, with the node of the upper snubber/filter circuit **230A** being connected to a low side of the lower snubber/filter circuit **230B** through snubber diode **237B** and the node of the lower snubber/filter circuit **230B** being connected to the high side of the upper snubber/filter circuit **230A** through snubber diode **237A**.

Each of the snubber/filter circuits **230A**, **230B** further includes a filter inductor **234A**, **234B**. The filter inductor **234A**, **234B** of the upper snubber/filter circuit **230A** is on a low side of the snubber/filter circuit **230A**, and the filter inductor **234B** of the lower snubber/filter circuit **230B** is on a high side of the snubber/filter circuit **230B**. Each of the filter inductors **234A**, **234B** is connected to a midpoint node **250**. The midpoint node **250** is connected to each of the high and low voltage outputs **240A**, **240B** via corresponding substantially identical capacitors **252**, such that the capacitors **252** define a voltage differential between the high and low voltage outputs **240A**, **240B**. In some examples, the connections used for the capacitors **252**, as well as the rectifier sections **220A**, **220B**, are low impedance connections.

Mirroring the rectifier sections **210A**, **210B**, as described above, facilitates the inclusion of the snubber diodes **237A**, **237B** in the recirculation circuit **232**. The snubber diodes **237A**, **237B** in turn recirculate the energy from each snubber/filter circuit **230A**, **230B** during the process of clamping voltage spikes into the opposite, mirrored, snubber/filter circuit **230A**, **230B**. By recirculating the energy, substantially less energy is required to be dissipated and no active switching is required in the snubber/filter circuits **230A**, **230B**. The snubber diodes **237A**, **237B** in the recirculation circuit **232** suppress the voltage spikes appearing at the outputs of full bridge rectifiers **220A**, **220B** by transferring energy into the snubber capacitors **235A**, **235B**. Diodes **233A**, **233B** reset the snubber capacitor **235A**, **235B** voltages during the time intervals when the voltages across transformer windings **224A**, **224B** are essentially zero by transferring energy stored in the snubber capacitors **235A**, **235B** to the output terminals **240A** and **240B**. In some

examples, the mirrored rectifier sections **210** are included in a circuit having low-inductance connections.

By recirculating the current through mirrored snubber/filter sections **230A**, **230B**, as in the example of FIGS. **1** and **2**, recirculation of energy can be achieved without requiring an additional recirculation inductor in each snubber/filter circuit **230A**, **230B**. This reduces the weight and cost, and can be particularly beneficial for applications having tight weight allowances and/or requiring substantial certification of each component, such as a satellite or other space based circuit.

In some applications, a greater range of operation at full output power than can be achieved via a single bridge driver **150** is required. Exemplary systems capable of achieving the greater full power operating range include dual full bridge converters capable of being operated in either a known Pulse Width Modulation (PWM) mode or a known phase shifted bridge mode.

FIG. **3** schematically illustrates an example dual full bridge converter **300** including two full bridge drivers **350X**, **350Y** and two sets of mirrored rectifier sections **310**, **330**. Full bridge driver **350X** drives a transformer X, and full bridge driver **350Y** drives a transformer Y thereby forming a multi-phase power system. Each of the sets of mirrored rectifier sections **310**, **330** are substantially similar to the rectifier sections **210A** and **210B** of FIG. **2**, with the exception that the bridge circuits **320** are multi-phase bridge circuits that each rectify the voltages from the two transformers X and Y, whereas the bridge circuits **220A** and **220B** of FIG. **2** are single-phase bridge circuits.

Each of the mirrored snubber/filter sections **360A**, **360B** are connected to a corresponding bridge circuit **320**, and are configured identical to the snubber/filter circuits **230A**, **230B** illustrated in FIG. **2**. To increase the voltage between the output nodes **340**, the two sets of mirrored rectifier sections **310**, **330** are connected in series, with the low side of **310** being connected to the high side output of **330**, resulting in a voltage output that is about twice the voltage output of either mirrored rectifier section individually. In another example, only one of mirrored rectifier sections **310**, **330** is connected between output terminals **340**, similar to the arrangement shown in FIG. **2**.

In yet further examples, additional rectifier sections, beyond the two rectifier sections **310**, **330** illustrated in FIG. **3** can be utilized in series, thereby providing additional voltage increases at the output nodes **340**. Similarly, multiple circuits of the types shown in FIGS. **1** and **2** may be connected in series to provide a higher output voltage.

When high output currents at lower output voltages are desired, full bridge drivers **350X** and **350Y** are operated in a PWM mode with the voltage waveforms across transformers X and Y being out of phase. This causes the currents produced by bridge rectifiers **320** to be equal to the sum of the currents produced by the individual secondary windings of transformers X and Y that are connected to each bridge rectifier. When operating in a PWM mode, the voltage between output nodes **340** is regulated by adjusting duty cycle of full bridge drivers **350X**, **350Y**.

When high output voltages at lower output currents are desired, full bridge drivers **350X**, **350Y** are operated in a phase shifted bridge mode with the voltages across transformers X and Y being at nearly 100 percent duty cycle, but with an adjustable phase relationship. Maximum output voltage occurs when full bridge drivers **350X**, **350Y** are operated in phase and the voltages across the secondary windings of transformers X and Y add to produce about twice the voltage between output nodes **340** than can be

produced when operating in a PWM mode with the voltage waveforms across transformers X and Y being out of phase.

In yet further examples, full bridge drivers **350X** and **350Y** include inductors **351** and diodes **352**. Inductors **351** can be used to facilitate a known highly-efficient mode of operation commonly called zero-volt-switching. When the duty cycle of the full-bridge drivers falls below 50 percent, inductors **351** can resonate with snubber capacitors **361**, which reduces the effectiveness of the snubbers in clamping the output voltages of rectifiers **320**. Including clamping diodes **352** in the full bridge drivers limits the voltage across the primary windings of transformers X and Y to the input voltage supplied to the bridge drivers, and thereby restores the effectiveness of the snubbing while still allowing zero-volt-switching to occur.

Transformers can be designed to have high leakage inductances in order to facilitate zero-voltage switching as an alternative to using separate primary inductors **351**, but the high leakage inductance implementation does not allow clamping diodes **352** to be used, and therefore it provides less optimal snubber effectiveness when the duty cycle is below fifty percent.

In yet further examples, driver **150** in FIG. **1** may be implemented with a full bridge driver utilizing clamping diodes and an inductor in an arrangement to similar to diodes **352** and inductor **351** in **350X** and **350Y** to enhance the effectiveness of the snubber circuits in FIGS. **1** and **2** for operating conditions in which the duty cycle is less than 50 percent.

In some examples, filter inductors **234A** and **234B** are coupled as shown by the polarity dots as shown in FIG. **2**. In some further examples, the filter inductors shown in FIG. **3** that have matching polarity dots are coupled with the indicated polarities.

It is further understood that any of the above described concepts can be used alone or in combination with any or all of the other above described concepts. Although an embodiment of this invention has been disclosed, a worker of ordinary skill in this art would recognize that certain modifications would come within the scope of this invention. For that reason, the following claims should be studied to determine the true scope and content of this invention.

The invention claimed is:

1. A power converter comprising:

a first rectifier circuit having a pair of first rectifier circuit output terminals and a second rectifier circuit having a pair of second rectifier circuit output terminals;

a snubber circuit comprising a first diode and a first capacitor connected to each other at a first node, the first diode and the first capacitor being connected in series and the series connected first diode and first capacitor connect the pair of first rectifier circuit output terminals, a second diode and a second capacitor connected to each other at a second node, the second diode and the second capacitor being connected in series and the series connected second diode and second capacitor connect the pair of second rectifier circuit output terminals, a third diode connecting the first node to a low voltage output of the pair of second rectifier output terminals, and a fourth diode connecting the second node to a high voltage output of the pair of first rectifier output terminals.

2. The power converter of claim **1**, wherein the first capacitor is connected to the one of the pair of first terminals not connected to the third diode and the second capacitor is connected to the one of the pair of second terminals not connected to the fourth diode.

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3. The power converter of claim 1, wherein said snubber circuit further includes a first filter inductor connecting the one of the pair of first terminals not connected to the third diode to a midpoint node, and a second filter inductor connecting the one of the pair of second terminals not connected to the fourth diode to the midpoint node. 5

4. The power converter of claim 1, wherein each of the first rectifier circuit and the second rectifier circuit are one of a full bridge rectifier and a center tapped rectifier.

5. The power converter of claim 1, wherein the each of the first rectifier and the second rectifier comprises a plurality of silicon diodes. 10

6. The power converter of claim 1, wherein each of the first rectifier circuit and the second rectifier circuit rectify currents from transformers driven by a multi-phase power system. 15

7. The power converter of claim 6 in which the multi-phase power system includes drivers that may be selectively operated in either a pulse width modulated mode or a phase shifted bridge mode.

8. The power converter of claim 1, comprising a plurality of pairs of rectifier sections wherein each of the first rectifier circuit and the second rectifier circuit is substantially identical to each other corresponding rectifier section. 20

9. The power converter of claim 1 in which each rectifier receives power from at least one transformer that has a primary winding. 25

10. The power converter of claim 9 in which the voltage across each primary winding is limited by clamping diodes.

11. The power converter of claim 1, wherein the first node is a node of an upper portion of the snubber circuit and is connected to a low side of a lower portion of the snubber circuit through the third diode and the node of the lower snubber circuit is connected to a high side of the upper snubber circuit through the fourth diode, and a midpoint node connects a low voltage output of the first rectifier circuit to a high voltage output of the second rectifier circuit. 30 35

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12. A method for reducing voltage spikes in a power converter comprising:

recirculating snubber energy through a snubber circuit comprising a first diode and a first capacitor connected to each other at a first node, the first diode and the first capacitor being connected in series and the series connected first diode and first capacitor connecting a pair of first rectifier circuit output terminals, a second diode and a second capacitor connected to each other at a second node, the second diode and the second capacitor being connected in series and the series connected second diode and second capacitor connecting a pair of second rectifier circuit output terminals, a third diode connecting the first node to one of the pair of second rectifier output terminals, and a fourth diode connecting the second node to one of the pair of first rectifier output terminals.

13. The method of claim 12, further comprising filtering a voltage between a high-voltage output node and a low-voltage output node using a third capacitor connecting the high voltage output node to a midpoint node and a fourth capacitor connecting the low voltage output node to the midpoint node.

14. The method of claim 12, wherein the first capacitor and the second capacitor have approximately the same capacitance.

15. the method of claim 12, wherein the first node is a node of an upper portion of the snubber circuit and is connected to a low side of a lower portion of the snubber circuit through the third diode and the node of the lower snubber circuit is connected to a high side of the upper snubber circuit through the fourth diode, and a midpoint node connects a low voltage output of a first rectifier circuit to a high voltage output of a second rectifier circuit.

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